Low Current LED Driver

This device is designed to replace discrete solutions for driving LEDs in AC/DC high voltage applications (up to 200 V). An external resistor allows the circuit designer to set the drive current for different LED arrays. This discrete integration technology eliminates individual components by combining them into a single package, which results in a significant reduction of both system cost and board space. The device is a small surface mount package (SO–8).

Features

- Supplies Constant LED Current for Varying Input Voltages
- External Resistor Allows Designer to Set Current up to 70 mA
- Offered in Surface Mount Package Technology (SO-8)
- Pb-Free Package is Available

Benefits

- Maintains a Constant Light Output During Battery Drain
- One Device can be used for Many Different LED Products
- Reduces Board Space and Component Count
- Simplifies Circuit and System Designs

Typical Applications

- Portables: For Battery Back–up Applications, also Simple Ni–CAD Battery Charging
- Industrial: General Lighting Applications and Small Appliances
- Automotive: Tail Lights, Directional Lights, Back-up Light, Dome Light

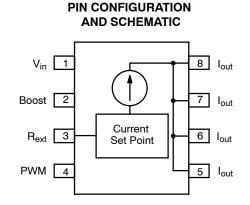
PIN FUNCTION DESCRIPTION

Pin	Symbol	Description		
1	V _{in}	Positive input voltage to the device		
2	Boost	This pin may be used to drive an external transistor as described in the App Note AND8198/D.		
3	R _{ext}	An external resistor between R _{ext} and V _{in} pins sets different current levels for different application nee		
4	PWM	For high voltage applications (higher than 48 V), pin 4 is connected to the LEDs array. For low voltage applications (lower than 48 V), pin 4 is connected to ground.		
5, 6, 7, 8	I _{out}	The LEDs are connected from these pins to ground		

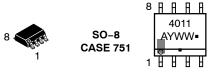


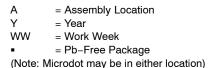
ON Semiconductor®

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ORDERING INFORMATION

Device	Package	Shipping [†]
NUD4011DR2	SO-8	2500 / Tape & Reel
NUD4011DR2G	SO-8 (Pb-Free)	2500 / Tape & Reel

[†]For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specification Brochure, BRD8011/D.

MAXIMUM RATINGS ($T_A = 25^{\circ}C$ unless otherwise noted)

Rating	Symbol	Value	Unit
Input Voltage	V _{in}	200	V
Output Current (For $V_{drop} \le 16 \text{ V}$) (Note 1)	l _{out}	70	mA
Output Voltage	V _{out}	198	V
Human Body Model (HBM)	ESD	500	V

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability. 1. $V_{drop} = V_{in} - 0.7 V - V_{LEDs}$.

THERMAL CHARACTERISTICS

Characteristic	Symbol	Value	Unit
Operating Ambient Temperature	T _A	-40 to +125	°C
Maximum Junction Temperature	TJ	150	°C
Storage Temperature	T _{STG}	-55 to +150	°C
Total Power Dissipation (Note 2) Derating above 25°C (Figure 3)	PD	1.13 9.0	W mW/°C
Thermal Resistance, Junction-to-Ambient (Note 2)	$R_{ hetaJA}$	110	°C/W
Thermal Resistance, Junction-to-Lead (Note 2)	$R_{ ext{ heta}JL}$	77	°C/W

2. Mounted on FR-4 board, 2 in sq pad, 1 oz coverage.

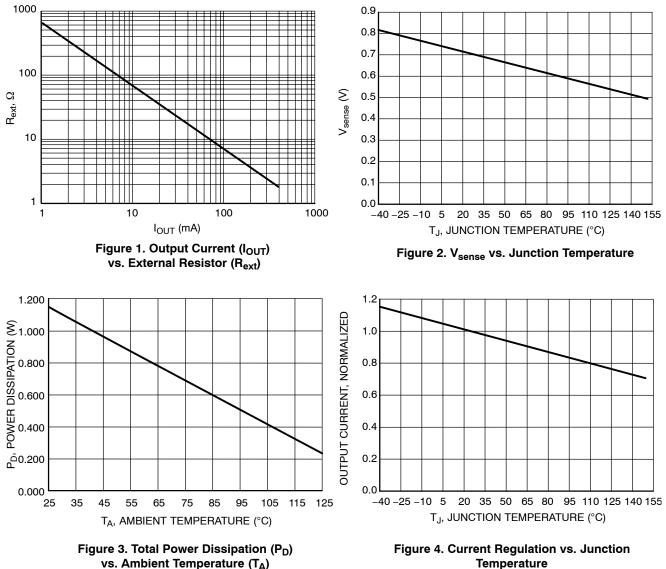
ELECTRICAL CHARACTERISTICS (T_A = 25°C unless otherwise noted)

Characteristic	Symbol	Min	Тур	Max	Unit
Output Current1 (Note 3) (V_{in} = 120 Vdc, R_{ext} = 24 Ω , V_{LEDs} = 90 V)	l _{out1}	26.0	27.5	29.5	mA
Output Current2 (Note 3) (V_{in} = 200 Vdc, R_{ext} = 68 Ω , V_{LEDs} = 120 V)	I _{out2}	11.5	14.0	15.5	mA
Bias Current (V _{in} = 120 Vdc, R _{ext} = Open, R _{shunt} = 80 kΩ)	I _{Bias}	-	1.1	2.0	mA
Voltage Overhead (Note 4)	V _{over}	5.0	-	-	V

3. Device's pin 4 connected to the LEDs array (as shown in Figure 5). 4. $V_{over} = V_{in} - V_{LEDs}$.

TYPICAL PERFORMANCE CURVES

 $(T_A = 25^{\circ}C \text{ unless otherwise noted})$



vs. Ambient Temperature (T_A)

APPLICATION INFORMATION

Design Guide for DC Applications

- 1. Define LED's current: a. $I_{LED} = 30 \text{ mA}$
- 2. Calculate Resistor Value for R_{ext} : a. $R_{ext} = V_{sense}$ (see Figure 2) / I_{LED} b. $R_{ext} = 0.7(T_J = 25 \text{ °C}) / 0.030 = 24 \Omega$
- 3. Define V_{in}:
 a. Per example in Figure 5, V_{in} = 120 Vdc
- 4. Define V_{LED} @ I_{LED} per LED supplier's data sheet: per example in Figure 5,
 a. V_{LED} = 3.0 V (30 LEDs in series)
 b. V_{LEDs} = 90 V
- 5. Calculate Vdrop across the NUD4001 device:
 - a. $V_{drop} = V_{in} V_{sense} V_{LEDs}$
 - b. $V_{drop} = 120 \text{ V} 0.7 \text{ V} 90 \text{ V}$
 - c. $V_{drop} = 29.3 V$
- 6. Calculate Power Dissipation on the NUD4001 device's driver:
 - a. $P_{D_{driver}} = V_{drop} * I_{out}$ b. $P_{D_{driver}} = 29.3 V \times 0.030 A$
 - c. $P_{D_{driver}} = 0.879 \text{ W}$
- 7. Establish Power Dissipation on the NUD4001 device's control circuit per below formula: a. $P_{D_control} = (V_{in} - 1.4 - V_{LEDs})^2 / 20,000$ b. $P_{D_control} = 0.040$ W
- 8. Calculate Total Power Dissipation on the device:
 a. P_{D_total} = P_{D_driver} + P_{D_control}
 b. P_{D total} = 0.879 W + 0.040 W = 0.919 W
- 9. If $P_{D_{total}} > 1.13$ W (or derated value per Figure 3), then select the most appropriate recourse and repeat steps 1–8:
 - a. Reduce V_{in}
 - b. Reconfigure LED array to reduce $V_{drop} \label{eq:configure}$
 - c. Reduce I_{out} by increasing R_{ext}
 - d. Use external resistors or parallel device's configuration
- 10. Calculate the junction temperature using the thermal information on Page 8 and refer to Figure 4 to check the output current drop due to the calculated junction temperature. If desired, compensate it by adjusting the value of R_{ext} .

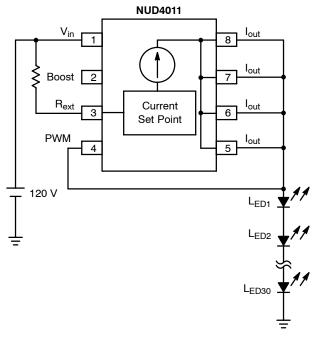


Figure 5. 120 V Application (Series LED's Array)

APPLICATION INFORMATION (continued)

Design Guide for AC Applications

1. Define LED's current: a. $I_{LED} = 30 \text{ mA}$

- 2. Define V_{in}: a. Per example in Figure 5, $V_{in} = 120$ Vac
- 3. Define V_{LED} @ I_{LED} per LED supplier's data sheet:
 - a. Per example in Figure 6, $V_{LED} = 3.0 V (30 LEDs in series)$ $V_{LEDs} = 90 V$
- 4. Calculate Resistor Value for Rext:
 - The calculation of the Rext for AC applications is totally different than for DC. This is because current conduction only occurs during the time that the ac cycles' amplitude is higher than V_{LEDs}. Therefore Rext calculation is now dependent on the peak current value and the conduction time.
 - a. Calculate θ for V_{LEDs} = 90 V:

$$V = V_{peak} \times \sin \theta$$

90 V = (120 × $\sqrt{2}$) × Sin θ
 θ = 32.027°

b. Calculate conduction time for $\theta = 32.027^{\circ}$. For a sinuousoidal waveform Vpeak happens at $\theta = 90^{\circ}$. This translates to 4.165 ms in time for a 60 Hz frequency, therefore 32.027° is 1.48 ms and finally:

Conduction time = $(4.165 \text{ ms} - 1.48 \text{ ms}) \times 2$ = 5.37 ms

c. Calculate the I_{peak} needed for $I_{(avg)} = 30$ mA Since a full bridge rectifier is being used (per Figure 6), the frequency of the voltage signal applied to the NUD4011 device is now 120 Hz. To simplify the calculation, it is assumed that the 120 Hz waveform is square shaped so that the following formula can be used:

 $I_{(avg)} = I_{peak} \times duty cycle;$

If 8.33 ms is 100% duty cycle, then 5.37 ms is 64.46%, then:

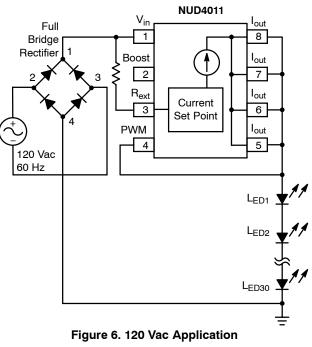
$$I_{peak} = I_{(avg)} / duty cycle$$

$$I_{peak} = 30 \text{ mA} / 0.645 = 46 \text{ mA}$$

d. Calculate Rext

$$R_{ext} = 0.7 \text{ V} / I_{peak}$$
$$R_{ext} = 15.21 \Omega$$

- 5. Calculate V_{drop} across the NUD4011 device:
 - a. $V_{drop} = V_{in} V_{sense} V_{LEDs}$
 - b. $V_{drop} = 120 V 0.7 V 90 V$
 - c. $V_{drop} = 29.3 V$





- 6. Calculate Power Dissipation on the NUD4011 device's driver:

 - a. $P_{D_driver} = V_{drop} * I_{(avg)}$ b. $P_{D_driver} = 29.3 V \times 0.030 A$
 - c. $P_D driver = 0.879 W$
- 7. Establish Power Dissipation on the NUD4011device's control circuit per below formula:

a.
$$P_{D_{control}} = (V_{in} - 1.4 - V_{LEDs})^2 / 20,000$$

b. $P_{D_{control}} = 0.040 \text{ W}$

- 8. Calculate Total Power Dissipation on the device:
 - a. $P_{D \text{ total}} = P_{D_{driver}} + P_{D_{control}}$
 - b. $P_{D \text{ total}} = 0.879 \text{ W} + 0.040 \text{ W} = 0.919 \text{ W}$
- 9. If P_D total > 1.13 W (or derated value per Figure 3), then select the most appropriate recourse and repeat steps 1-8:
 - a. Reduce Vin
 - b. Reconfigure LED array to reduce Vdrop
 - c. Reduce Iout by increasing Rext
 - d. Use external resistors or parallel device's configuration
- 10. Calculate the junction temperature using the thermal information on Page 8 and refer to Figure 4 to check the output current drop due to the calculated junction temperature. If desired, compensate it by adjusting the value of Rext.



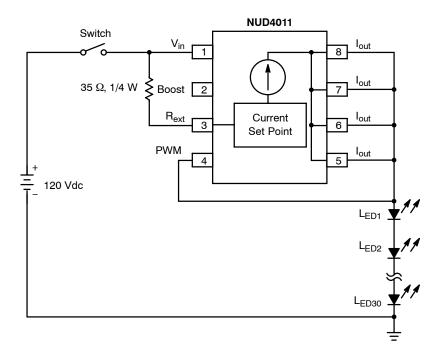


Figure 7. 120 Vdc Application Circuit for a Series Array of 30 LEDs (3.0 V, 20 mA)

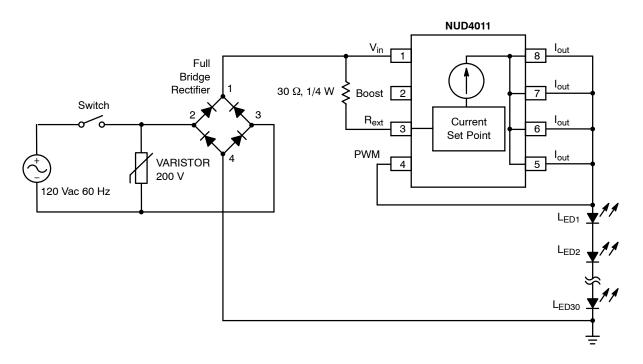


Figure 8. 120 Vac Application Circuit for a Series Array of 30 LEDs (3.0 V, 20 mA)

TYPICAL APPLICATION CIRCUITS (continued)

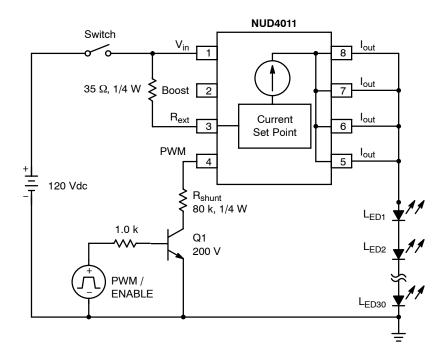


Figure 9. 120 Vdc Application with PWM / Enable Function, 30 LEDs in Series (3.0 V, 20 mA)

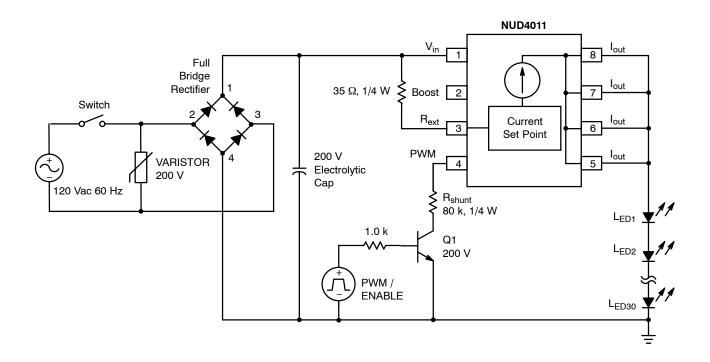


Figure 10. 120 Vac Application with PWM / Enable Function, 30 LEDs in Series (3.0 V, 20 mA)

THERMAL INFORMATION

NUD4011 Power Dissipation

The power dissipation of the SO–8 is a function of the pad size. This can vary from the minimum pad size for soldering to a pad size given for maximum power dissipation. Power dissipation for a surface mount device is determined by $T_{J(max)}$, the maximum rated junction temperature of the die, $R_{\theta JA}$, the thermal resistance from the device junction to ambient, and the operating temperature, T_A . Using the values provided on the data sheet for the SO–8 package, P_D can be calculated as follows:

$$P_{D} = \frac{T_{Jmax} - T_{A}}{R_{\theta}JA}$$

The values for the equation are found in the maximum ratings table on the data sheet. Substituting these values into the equation for an ambient temperature T_A of 25°C, one can calculate the power dissipation of the device which in this case is 1.13 W.

$$P_{D} = \frac{150^{\circ}C - 25^{\circ}C}{110^{\circ}C} = 1.13 \text{ W}$$

The 110°C/W for the SO–8 package assumes the use of a FR–4 copper board with an area of 2 square inches with 2 oz coverage to achieve a power dissipation of 1.13 W. There are other alternatives to achieving higher dissipation from the SOIC package. One of them is to increase the copper area to

reduce the thermal resistance. Figure 11 shows how the thermal resistance changes for different copper areas. Another alternative would be to use a ceramic substrate or an aluminum core board such as Thermal Clad®. Using a board material such as Thermal Clad or an aluminum core board, the power dissipation can be even doubled using the same footprint.

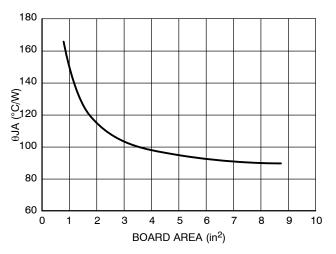


Figure 11. 0JA versus Board Area

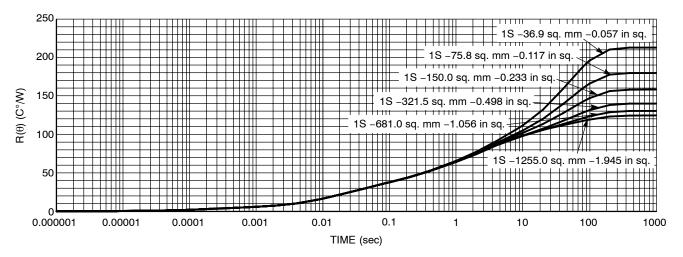
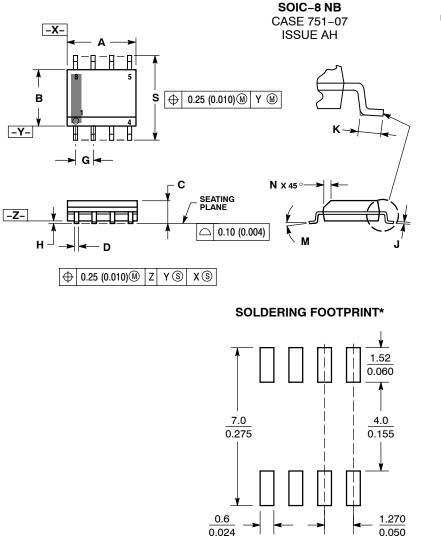


Figure 12. Transient Thermal Response

PACKAGE DIMENSIONS



NOTES

- 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
- CONTROLLING DIMENSION: MILLIMETER. DIMENSION A AND B DO NOT INCLUDE 2 З.
- MOLD PROTRUSION. MAXIMUM MOLD PROTRUSION 0.15 (0.006) 4. PER SIDE. DIMENSION D DOES NOT INCLUDE DAMBAR 5.
- PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.127 (0.005) TOTAL IN EXCESS OF THE D DIMENSION AT
- MAXIMUM MATERIAL CONDITION. 751–01 THRU 751–06 ARE OBSOLETE. NEW 6 STANDARD IS 751-07.

	MILLIN	IETERS	INCHES		
DIM	MIN	MAX	MIN	MAX	
Α	4.80	5.00	0.189	0.197	
В	3.80	4.00	0.150	0.157	
С	1.35	1.75	0.053	0.069	
D	0.33	0.51	0.013	0.020	
G	1.27	7 BSC	0.050 BSC		
н	0.10	0.25	0.004	0.010	
J	0.19	0.25	0.007	0.010	
ĸ	0.40	1.27	0.016	0.050	
м	0 °	8 °	0 °	8 °	
Ν	0.25	0.50	0.010	0.020	
S	5.80	6.20	0.228	0.244	

 $\left(\frac{mm}{inches}\right)$ SCALE 6:1 *For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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